Observation of injection locking in an optomechanical rf oscillator

Mani Hossein-Zadeha and Kerry J. Vahala

Department of Applied Physics, California Institute of Technology, Pasadena, California 91125, USA

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Injection locking of a radiation-pressure optomechanical oscillator is demonstrated through external modulation of the optical pump power near the optomechanical oscillation frequency. It is shown that the frequency and phase of a microtoroidal optomechanical oscillator can be locked to those of an electronic oscillator (or any other signal) that can modulate the optical input power and whose frequency is within the lock range. © 2008 American Institute of Physics.

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Injection locking is a well-known effect in both self-sustained electronic and photonic oscillators (lasers). When a periodic signal with a frequency close to the oscillation frequency and large enough amplitude is injected into a self-sustained oscillator, the phase and frequency of the oscillator can be locked to that of the injected signal. Here this phenomenon is investigated in an optomechanical oscillator (OMO). OMOs are driven by radiation pressure and rely upon “dynamic back action” created when a continuous wave (cw) optical pump is blue-detuned relative to a resonance of an optical resonator that also features high-Q mechanical modes. The OMOs of this study are based on high-Q silica microtoroids. The high optical $Q$ factor and the unique geometry of toroid resonator (that enables efficient coupling between optical and mechanical degrees of freedom through radiation pressure) lead to self-sustained rf mechanical oscillations of the microtoroid structure (even to gigahertz frequencies). Characterization of the phase noise and oscillation frequency have confirmed that the microtoroid OMO is potentially important in certain rf-photonic systems. We demonstrate that partial amplitude modulation of the optical input power can lock both frequency and phase of the optomechanical oscillation to that of the external oscillator (used to modulate the input optical power). Preliminary experimental results confirm that injection locking in an OMO exhibits the characteristics of injection locking in electronic oscillators.

Figure 1 shows the experimental arrangement used to study injection locking in the microtoroid OMO. The optical power from a tunable laser passes through a Mach–Zehnder (MZ) modulator and is coupled into and out of the microtoroid optical resonator using a fiber-taper coupler. The amplitude of the optical input power ($P_{in}$) is partially modulated by a single tone rf signal from a tunable rf synthesizer applied on the MZ modulator. The modulation index is thereby used to control the strength of the weaker injection-locking signal (modulated fraction of $P_{in}$) in comparison to the pump (cw fraction of $P_{in}$). The spectrum of optical power that is coupled out of the microtoroid is then analyzed in a rf spectrum analyzer. Also, the phase of the output signal is compared to that of the electronic input signal (injected signal) using a lock-in amplifier. When the amplitude of the injected signal is large enough and its frequency ($f_{inj}$) is close to the optomechanical oscillation frequency ($f_{OMO}$), we observe injection locking of the OMO. Figure 2(a) shows the rf spectrum of the output power in the absence (gray trace) and presence (black trace) of modulation (injection). The microtoroid OMO chosen for this experiment had a mechanical frequency of about 84.1 MHz. In this case the frequency of the injected signal is 500 Hz smaller than the optomechanical oscillation frequency. The dashed trace is the rf spectrum of the optical input power when the external modulation is ON. In all experiments the laser power and amplitude modulation depth are chosen such that the cw optical input power is larger than the threshold power for optomechanical oscillation ($P_{th}$) but small enough to keep the oscillation in the linear regime (where the second harmonic is at least 15 dB smaller than the fundamental frequency). It is apparent that the presence of the modulation pulls $f_{OMO}$ toward $f_{inj}$ and locks the two signals. As shown in Fig. 2(b) injection locking can be used to tune the optomechanical oscillation frequency simply by tuning $f_{inj}$. At a given ratio between modulation amplitude of the input signal and amplitude of the optomechanical oscillation imposed on the optical output ($A_{inj}/A_{OMO}$), locking occurs within a limited bandwidth around $f_{OMO}$ (known as lock range). Similar to an electronic oscillator, for tuning slightly above and below the edge of lock range, the oscillator is quasiloocked and the rf spectrum consists of a series of closely spaced decaying beat frequencies in the vicinity of $f_{OMO}$ [Fig. 2(c)]. Based on the theoretical prediction using the general theory of injection locking for self-sustained oscillators, the lock range can be written as

![Figure 1. Schematic diagram of the experimental arrangement used to study injection locking in a microtoroid OMO.](image-url)
where $\Delta f_{\text{lock}} = \Delta f_{\text{mech}} A_{\text{inj}}/A_{\text{OMO}} \left[ 1 - \left( \frac{A_{\text{inj}}}{A_{\text{OMO}}} \right)^2 \right]^{-1/2}$.

The temporal behavior of the phase difference at $f_{\text{OMO}} = f_{\text{inj}}$ in the presence (ON) and absence (OFF) of the injection signal on the MZ modulator. As evident from the trace, the phase difference remains close to zero when injection is ON and becomes random when injection is OFF. As a result, for $f_{\text{inj}}$ within lock range, the phase difference between the injected signal and the oscillation can be tuned by adjusting the frequency detuning.

The phase noise of the optomechanical oscillation under injection was also investigated, and as expected the presence of the locking signal improves the optomechanical oscillation phase noise. Figure 5 is the measured phase noise spectral density of the detected optical power for two frequency ranges (a) 0.01–10 kHz and (b) 10–1000 kHz. The
the vicinity of monic so that the frequency locking is clearly observable in intentionally detuned from the exact harmonic and subharmonic frequencies of the OMO to the modulating signal. The injected signals are the OMO at these frequencies can also lock the frequency of oscillation frequency. As evident from the graphs, injecting the fundamental oscillation frequency may open interesting frontiers in engineering of optomechanical rf oscillators and their applications. As an example, recently a photonic rf-receiver architecture based on the OMO has been demonstrated that can benefit from this phenomenon. In this design the locking between the optomechanical local oscillator and the received signal may relax the frequency stability requirement for the oscillator within the lock range. Injection locking of an OMO to an electronic rf oscillator enables combination of OMO with electronic devices and may have interesting applications in certain rf-photonics and micro-opto-electro-mechanical systems. Alternatively the nonelectronic nature of OMO makes them immune to electromagnetic interference and good candidates for all-optical systems. In this context injection locking can be used to lock two OMOs and improve the frequency stability and noise performance of the “slave” oscillator similar to atomic clocks as well as controlling optomechanical oscillations with atomic accuracy (by locking to atomic clocks).

In conclusion we have shown that injection locking technique can be used to lock the phase and frequency of an OMO to amplitude modulation of an input optical wave. This technique, widely used in electronic and photonic systems, may open interesting frontiers in engineering of optomechanical rf oscillators and their applications. As an example, recently a photonic rf-receiver architecture based on the OMO has been demonstrated that can benefit from this phenomenon. In this design the locking between the optomechanical local oscillator and the received signal may relax the frequency stability requirement for the oscillator within the lock range. Injection locking of an OMO to an electronic rf oscillator enables combination of OMO with electronic devices and may have interesting applications in certain rf-photonics and micro-opto-electro-mechanical systems. Alternatively the nonelectronic nature of OMO makes them immune to electromagnetic interference and good candidates for all-optical systems. In this context injection locking can be used to lock two OMOs and improve the frequency stability and noise performance of the “slave” oscillator similar to what is done in the optical domain with lasers (Improving the performance of a noisy high power laser with a narrow linewidth low power laser). Lastly injection locking is a useful feature in metrological applications where it can be used to synchronize multiple OMOs as well as controlling optomechanical oscillations with atomic accuracy (by locking to atomic clocks).

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FIG. 5. Measured phase noise spectral density of the detected optical power for two frequency offset ranges (a) 0.01–10 kHz and (b) 10–1000 kHz. The phase noise is measured for the free running OMO and also the OMO injection locked with $A_{\text{inj}}/A_{\text{OMO}}=0.1, 0.4,$ and 0.6.

FIG. 6. (a) Measured rf spectrum of the free running OMO (black trace) and the OMO locked to subharmonic and harmonic injected signals (gray traces). (b) and (c) are the spectrums of the harmonic and subharmonic injected signals, respectively.